

Interplanetary Departure From Circular Earth Parking Orbits (EPOs)

Consider a spacecraft initially in a circular Earth parking orbit (EPO) with height "H" above Earth's equatorial radius $R_E = 6378.136$ km. Two impulsive maneuver strategies are to be compared in departing this EPO for interplanetary space, assuming unperturbed conic geocentric motion (Earth's reduced mass, $\mu = 398,600.44$ km³/s²).

The first strategy, called "direct departure" (DD), simply increases EPO speed to achieve the specified Earth departure asymptotic speed v_{HE} (v_{HE}^2 is equivalent to Earth departure energy "C3"). The second strategy, called "Earth gravity assist" (EGA), is more complex than DD. Using EGA, a retrograde impulse first establishes a departure elliptical orbit (DEO) with apsis heights H and H_{MIN} , where H_{MIN} is the lowest practical orbit height for safe navigation and acceptable aerodynamic energy losses from a single perigee passage. All EGA data presented herein reflect $H_{MIN} = +200$ km. A posigrade impulse is then applied at DEO perigee to achieve v_{HE} and complete an EGA departure.

In comparing impulsive DD costs with those of EGA, the following quantities and formulae (obtained from conic section geometry and the energy integral) are relevant.

- 1) $r_{EPO} \equiv$ geocentric EPO radius = $R_E + H$

- 2) $v_{EPO} \equiv$ geocentric speed in the EPO = $\sqrt{\frac{\mu}{r_{EPO}}}$

- 3) $v_{DD} \equiv$ required geocentric speed to achieve v_{HE} at $r_{EPO} = \sqrt{C3 + \frac{2\mu}{r_{EPO}}}$

- 4) $\Delta v_{DD} \equiv$ impulse required to achieve v_{DD} directly from EPO (this will be a positive value to indicate a posigrade impulse) = $v_{DD} - v_{EPO}$

- 5) $a_{DEO} \equiv$ semi-major axis of DEO = $0.5 (r_{EPO} + r_{MIN})$

- 6) $v_1 \equiv$ geocentric DEO speed at $r_{EPO} = \sqrt{\mu \left(\frac{2}{r_{EPO}} - \frac{1}{a_{DEO}} \right)}$

- 7) $\Delta v_1 \equiv$ impulse required to transfer from EPO to DEO apogee (this will typically be a negative value to indicate a retrograde impulse) = $v_1 - v_{EPO}$

- 8) $v_2 \equiv$ geocentric DEO speed at $r_{MIN} = \sqrt{\mu \left(\frac{2}{r_{MIN}} - \frac{1}{a_{DEO}} \right)}$

- 9) $v_{EGA} \equiv$ required geocentric speed to achieve v_{HE} at $r_{MIN} = \sqrt{C3 + \frac{2\mu}{r_{MIN}}}$

- 10) $\Delta v_2 \equiv$ impulse required to achieve v_{EGA} from DEO perigee (this will typically be a positive value to indicate a posigrade impulse) = $v_{EGA} - v_2$

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- 11) $\Delta v_{\text{EGA}} \equiv$ total impulse required to achieve v_{EGA} from EPO after transfer to DEO perigee (this will be a positive value) = $|\Delta v_1| + |\Delta v_2|$
- 12) $\Delta\Delta v \equiv$ EGA impulse margin with respect to DD impulse = $\Delta v_{\text{DD}} - \Delta v_{\text{EGA}}$

Therefore, EGA is impulsively more efficient than DD only when $\Delta\Delta v$ is positive. Furthermore, because EGA requires loiter through at least half a DEO before Earth departure is achieved, DD is also clearly the superior choice from a timeline perspective when $\Delta\Delta v$ is negative or marginally positive.

For the parabolic escape case with $v_{\text{HE}} = 0$, Figure 1 plots $\Delta\Delta v$ as a function of H. There is no EPO for which Δv_{EGA} is less than Δv_{DD} in this case.

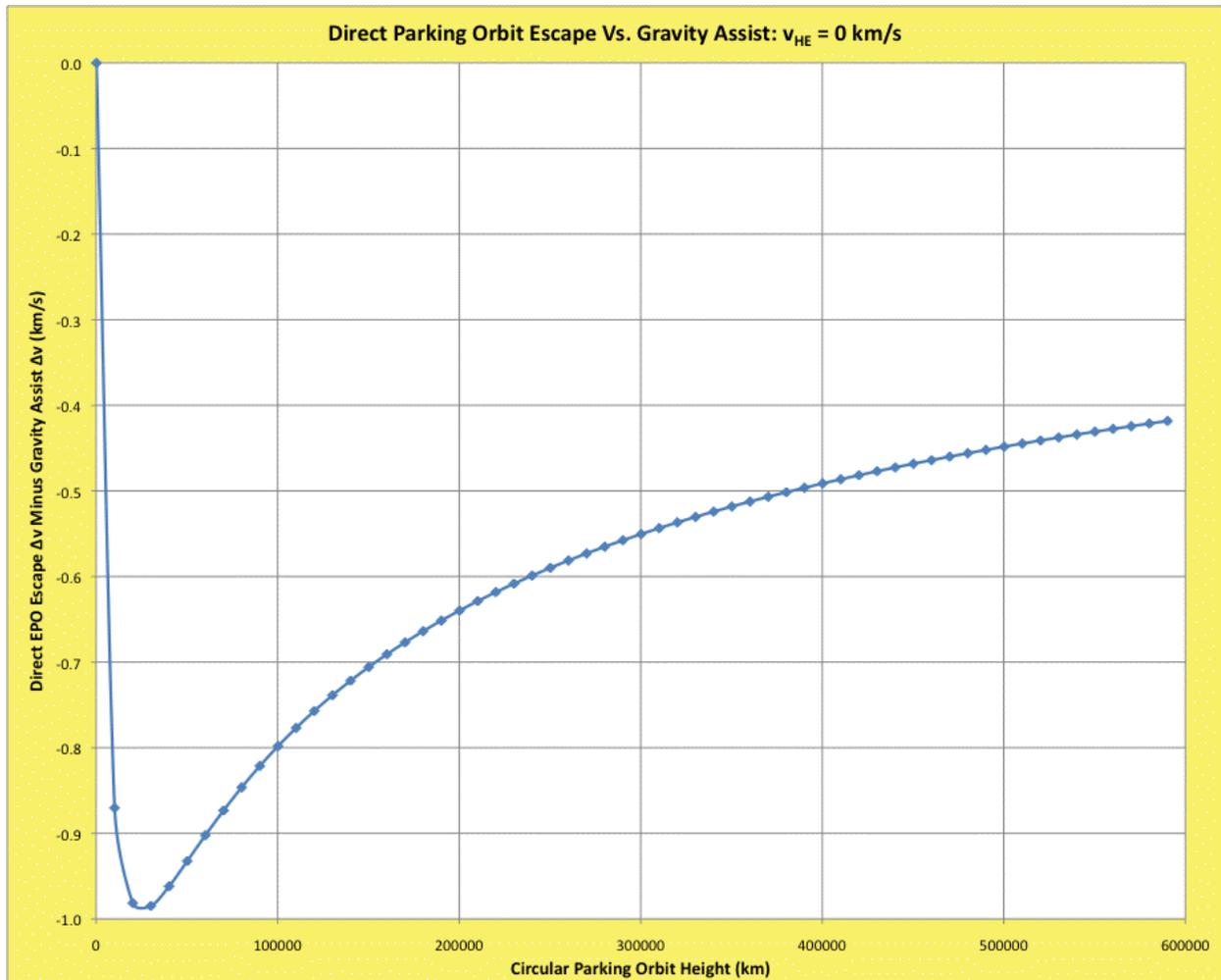


Figure 1: $\Delta\Delta v$ Versus H for Parabolic Earth Departure $v_{\text{HE}} = 0$

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When v_{HE} is increased to 2 km/s, the situation changes dramatically. As illustrated by Figure 2, Δv_{EGA} is less than Δv_{DD} when H exceeds +200,000 km, about halfway to the Moon's orbit.

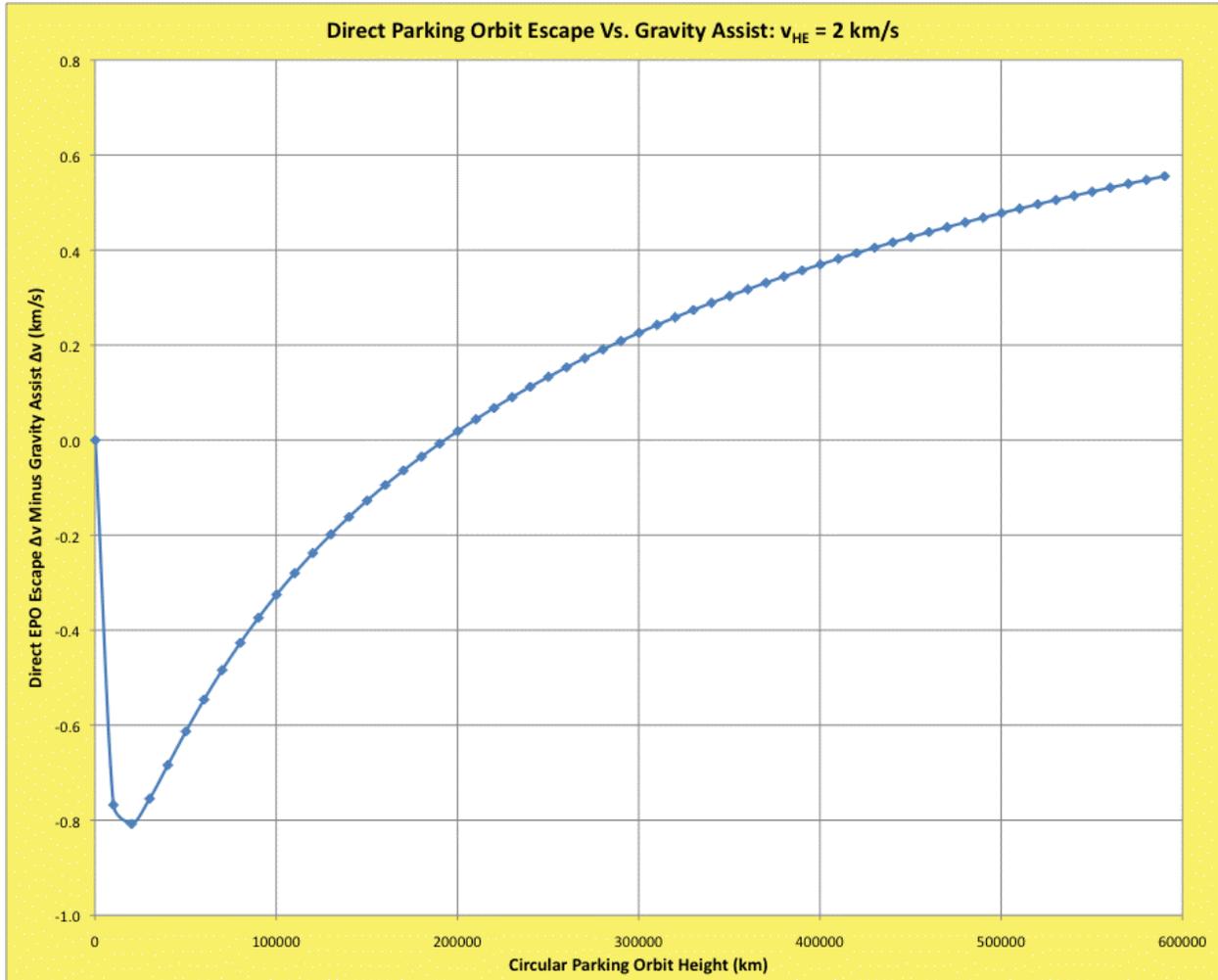


Figure 2: $\Delta\Delta v$ Versus H for Earth Departure $v_{HE} = 2$ km/s

Although conventional coasted trajectories to Venus and Mars typically call for v_{HE} well above 2 km/s, the most accessible near-Earth objects (NEOs) may require v_{HE} considerably less than 2 km/s. In these nearly parabolic Earth departures, a DD strategy may be preferable to EGA, even if EPO is in cis-lunar space with H near +400,000 km.